



Exam Information بيانات الامتحان					
2025/2024	العام الجامعي Academic year	الهندسة/ الهندسة الميكانيكية School of Engineering/ Mechanical Engineering		الكلية والقسم School & Dept.	
الأول	الفصل الدراسي Semester	Strength of Materials 1		اسم المادة Course name	
25 Feb 2025	تاريخ الامتحان Exam date	0904372		رقم المادة Course number	
13:00-15:00	وقت الامتحان Exam time	<input checked="" type="checkbox"/> نهائي Final	<input type="checkbox"/> منتصف الفصل Midterm	<input type="checkbox"/> أول/ثان 1 st /2 nd	نوع الامتحان Exam type
2 Hours	مدة الامتحان Exam duration	50		علامة الامتحان Exam Mark	
<input type="checkbox"/> ورقة إجابة منفصلة Separate answer sheet (bubble sheet)	نوع ورقة الإجابة Answer sheet type	<input checked="" type="checkbox"/> مقال مفتوح Open-ended		نوع الأسئلة Questions type	
<input type="checkbox"/> الورقة الأخيرة المرفقة بأوراق الأسئلة Last page attached to the questions papers		<input type="checkbox"/> موضوعي Close-ended			
<input checked="" type="checkbox"/> قلم رصاص Pencil <input checked="" type="checkbox"/> قلم حبر (أزرق/ أسود) Pen (blue/ black)	نوع قلم تدوين الإجابات Answering pen type	<input checked="" type="checkbox"/> آلة حاسبة Calculator <input type="checkbox"/> ورق فارغ Blank paper <input type="checkbox"/> أدوات أخرى وهي:		الأدوات التي يحتاجها الامتحان Exam required tools	

Student Information بيانات الطالب			
			اسم الطالب باللغة العربية (إجباري) Student's name in Arabic*
وقت المحاضرة Lecture time	رقم الشعبة Section no.	الرقم الجامعي (إجباري) Student's number*	
رقم الجلوس في الامتحان Exam seat no.		رقم الجلوس في المحاضرة Seat no. in lecture room	

Exam Instructions تعليمات الامتحان	
1. Read the exam information carefully and adhere to it: question types, answer sheet format, pen type, necessary tools, total exam marks, and exam duration.	1. قم بقراءة بيانات الامتحان بتمعن والتزم بها: نوع الأسئلة، ونوع ورقة الإجابة، ونوع القلم، والأدوات التي يحتاجها الامتحان، وعلامة الامتحان الكلية، ومدة الامتحان.
2. Ensure that all your question pages are available.	2. تحقق من توفر جميع صفحات الأسئلة لديك.
3. Do not place any exam-related materials close to your seat.	3. يمنع وضع المواد ذات الصلة بالامتحان قريبا من المقعد.
4. Mobile phones are prohibited and must be completely turned off, not in airplane/silent mode. Follow the supervisors' instructions regarding phones.	4. يحظر استخدام الهواتف النقالة ويتم إغلاقها بشكل تام وليس في وضع الطيران/الصامت، ويجب اتباع تعليمات المراقبين بشأن الهواتف.
5. Use of headphones or any type of smart devices (visual/auditory/sensory) is prohibited.	5. يحظر استخدام سماعات الرأس أو الأجهزة الذكية من أي نوع (البصرية/ السمعية/ الحسية).
6. Do not use/bring additional papers for the exam; you will be provided with the necessary papers if required during the exam.	6. يحظر استخدام/ إحضار أوراق إضافية للامتحان وسيتم تزويدك بالورق الذي تحتاجه إذا تطلب الامتحان ذلك.

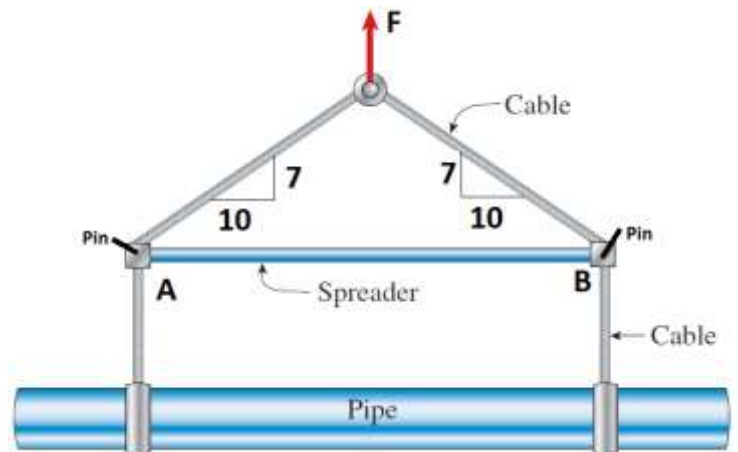
Exam Supervisor's Notes ملاحظات مراقب الامتحان
SN=4

The hoisting arrangement for lifting a large pipe is shown in the figure. The spreader is a steel tubular section with outer diameter ($10 \times SN$) mm and inner diameter ($10 \times SN - 10$) mm, its length is 2.8 m and its modulus of elasticity is 180 GPa.

Q1. Based upon a factor of safety of 2.25 with respect to Euler buckling of the spreader, what is the maximum weight of pipe that can be lifted? (Assume pinned conditions at the ends of the spreader.)

(a) 264460.78 (b) 76477.535 (c) 51600.22

(d) 25538.652 (e) 1153.51 (f) 4498.678



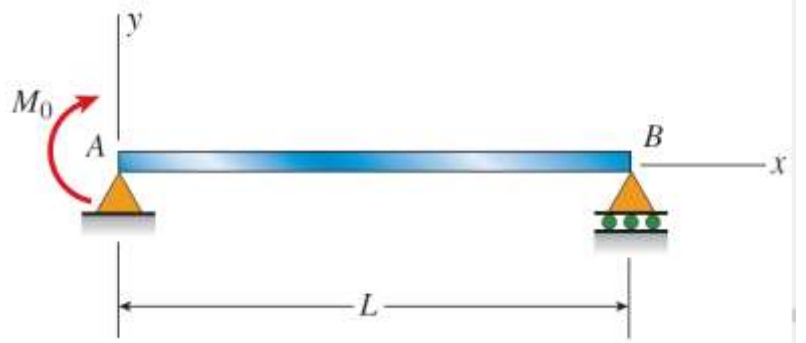
A simple beam AB of length $L= 2\text{m}$ is loaded by a couple $M_0 = 600 \text{ N.m}$ at the left-hand support with flexural rigidity $EI= 123456 \times \text{SN}$ (N.m^2).

Q2. The deflection (mm) at the mid-span ($x=L/2$) of the beam is:

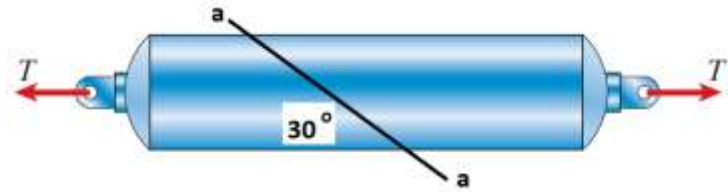
- (a)-1.215 (b)-0.17357 (c)-0.6075 (d)-0.2430 (e)-0.405 (f)-0.729

Q3. The slope (rad) at the right end of the beam (at B):

- (a)0.000231 (b)0.00054 (c)0.001157 (d)0.00405 (e)0.0027 (f)0.000324



A cylindrical tank having diameter $d=200\text{mm}$ is subjected to internal gas pressure $p = \text{SN}$ (MPa) and an external tensile load $T = 4.5 \text{ kN}$. Assuming that the cross sectional area of the cylindrical vessel is ($A = t \pi d$)



Q4. The minimum thickness t (mm) of the wall of the tank if the allowable normal stress at the outer boundary is 80 MPa.

- (a)2.5 (b)3.75 (c)7.5 (d)5 (e)6.25 (f)8.75

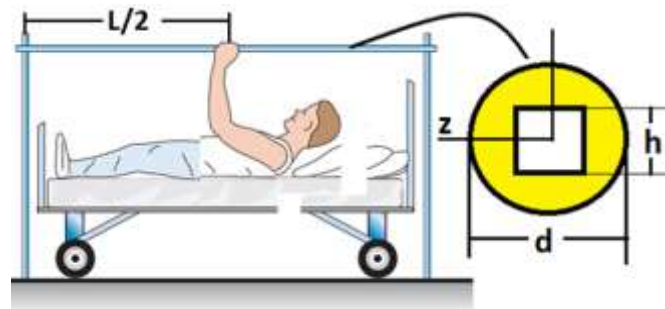
Q5. The minimum thickness t (mm) of the wall of the tank if the in-plane allowable shear stress $\left(\tau_{\max} = \left| \frac{\sigma_1 - \sigma_2}{2} \right| \right)$ at the outer boundary is 20 MPa.

- (a)8.571 (b)17.5 (c)15 (d)3.571 (e)6.071 (f)12.5

Q6. If the thickness of the wall is 10 mm, find the state of stresses (σ_a, τ_a) along the inclined plane a-a

- (a)43.929,10.515 (b)35.179,8.350 (c)61.429,14.845
 (d)17.679,4.020 (e)52.679,12.680 (f)26.429,6.185

A bar in a hospital room provides a means for patients to exercise while in bed. The bar is 2.2 m long and has a circular cross section with a square hole as shown, where $d = 20 \times SN$ mm. The design load is 1.2 kN applied at the midpoint of the bar.



Q7. If $h=30$ mm what is the second moment of inertia (mm^4) of the cross-section about z -axis.

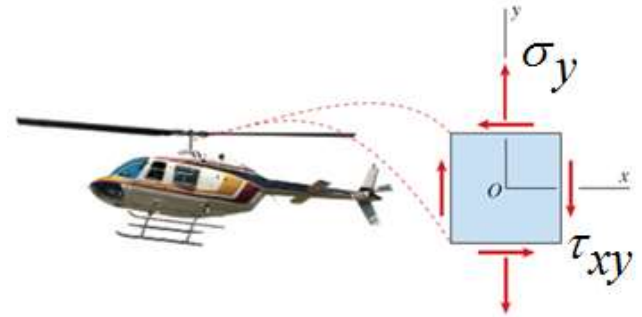
(a) 5.686×10^5 (b) 1.879×10^7 (c) 4.841×10^6

(d) 58163.706 (e) 3.210×10^7 (f) 1.943×10^6

Q8. If the allowable bending stress is 200 MPa, determine the minimum value of h (mm) (Assume that the ends of the bar are simply supported and its weight is negligible)

(a) 68.905 (b) 139.882 (c) 50.39 (d) 29.088 (e) 86.86 (f) 122.272

It is known that the stresses on the rotor shaft of a helicopter are: normal stress $\sigma_y = 10 \times SN$ MPa and shear stress $\tau_{xy} = -5 \times SN$ MPa. Using Mohr's circle, determine the following.



Q9. The largest principle stress (MPa) on the rotor is:

- (a)56.56 (b)49.49 (c)63.63 (d)21.21 (e)70.70 (f)35.35

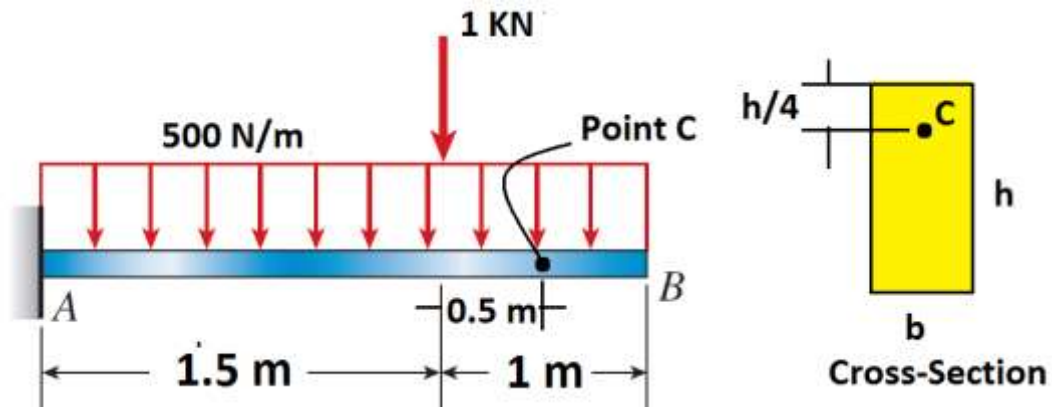
Q10. The maximum shear (MPa) stress in the shaft is:

- (a)108.63 (b)60.35 (c)120.71 (d)36.21 (e)96.56 (f)84.49

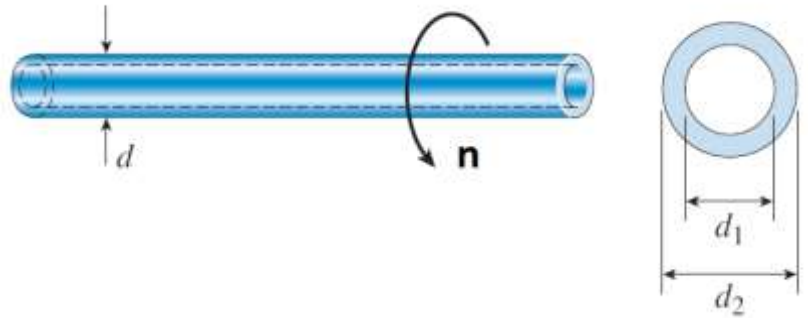
For the loaded cantilever beam shown if $h = 12 \times SN$ mm, and $b = 2 \times SN$ mm

Q11. The normal stress at point C (MPa) is
(a) 2.39 (b) 24.11 (c) 1.898 (d) 1.271 (e) 10.17 (f) 5.208

Q12. The shear stress at point C in MPa is
(a) 0.1831 (b) 0.732 (c) 0.468 (d) 0.325 (e) 0.239 (f) 1.302



A drive shaft is running at $n=400 \times \text{SN}$ rpm and the allowable shear stress in the shaft is $\tau_{allow} = 30 \text{ MPa}$.



- Q13.** If the outer diameter of the shaft is 60 mm and inner diameter 40 mm, the maximum power that can be transmitted by the hollow shaft is approximately (kW):
(a)42.768 (b)342.146 (c)85.536 (d)213.84 (e)299.378 (f)128.30
- Q14.** If this shaft is replaced by a solid shaft that have the same material and weight, the maximum power that can be transmitted by the solid shaft is approximately (kW):
(a)110.34 (b)66.20 (c)176.55 (d)44.138 (e)154.483 (f)22.069
- Q15.** Discuss the results of Q13 and Q14

Formula sheet, 2025

Prof. Ibrahim Abu-Alshaikh, JU, Mechanical Engineering Department

$$FS = \frac{\sigma_y}{\sigma_{allow}} \text{ and } FS = \frac{\tau_y}{\tau_{allow}}; \quad FS = \frac{\sigma_u}{\sigma_{allow}} \text{ and } FS = \frac{\tau_u}{\tau_{allow}}; \quad \sigma = E\varepsilon; \quad \tau = G\gamma$$

$$\sigma = \frac{F}{A}; \quad \tau_{aver} = \frac{F}{A}; \quad \delta = \sum_{i=1}^n \frac{P_i L_i}{E_i A_i}; \quad \delta = \frac{PL}{EA}; \quad \delta = \int_0^L \frac{P(x)}{EA(x)} dx; \quad \nu = \frac{\varepsilon_{lateral}}{\varepsilon_{longitudinal}}$$

$$\left. \begin{array}{l} \text{Power \& Torsion} \\ \left\{ \begin{array}{l} \phi = \frac{TL}{GI_p}; \quad I_p (\text{Solid Shaft of diam. } = d) = \frac{\pi d^4}{32}; \quad I_p (\text{Hollow Shaft } \left\{ \begin{array}{l} d_o : \text{outer diam.} \\ d_i : \text{inner diam.} \end{array} \right\}) = \frac{\pi (d_o^4 - d_i^4)}{32} \\ \tau_{max} = \frac{T(d/2)}{I_p}; \quad \tau = \frac{T\rho}{I_p} \left(\text{where } 0 \leq \rho \leq r = \frac{d}{2} \right); \quad G = \frac{E}{2(1+\nu)}; \quad P(\text{power}) = \omega T; \quad \omega = 2\pi f \end{array} \right\}$$

$$\frac{dV}{dx} = -q; \quad \frac{dM}{dx} = V \Leftrightarrow \left\{ \begin{array}{l} \int_A^B dV = V_A - V_B = - \int_A^B q dx = - (\text{Area of the loading diagram bt. A and B}) \\ \int_A^B dM = M_A - M_B = \int_A^B V dx = (\text{Area of the shear-force diagram bt. A and B}) \end{array} \right.$$

$$\kappa (\text{curvature}) = \frac{1}{\rho} = \frac{d\theta}{ds} = \frac{-\varepsilon_x}{y}; \quad \sigma_x = \frac{-M_z y}{I_z}; \quad \tau = \frac{VQ}{Ib}; \quad Q = \int y dA; \quad Q_{\text{Circle at NA}} = d^3 / 12$$

$$\left. \begin{array}{l} \text{Mohr's Circle, Stress Trans. \& Princ. Stresses} \\ \left\{ \begin{array}{l} \sigma_{x1}, \sigma_{y1} = \sigma_{aver} \pm \sigma_{diff} \cos(2\theta) \pm \tau_{xy} \sin(2\theta); \quad \sigma_{aver} = \frac{\sigma_x + \sigma_y}{2}; \quad \sigma_{diff} = \frac{\sigma_x - \sigma_y}{2} \\ \tau_{x1y1} = -\sigma_{diff} \sin(2\theta) + \tau_{xy} \cos(2\theta); \quad \sigma_{1,2} = \sigma_{aver} \pm R; \quad R = \sqrt{(\sigma_{diff})^2 + (\tau_{xy})^2} \end{array} \right\}$$

Hooke's law for plane stress & vessels:

$$\left\{ \begin{array}{l} \varepsilon_x = \frac{1}{E} (\sigma_x - \nu \sigma_y) \\ \varepsilon_y = \frac{1}{E} (\sigma_y - \nu \sigma_x) \\ \varepsilon_z = \frac{-\nu}{E} (\sigma_y + \sigma_x) \end{array} \right\} \left\{ \begin{array}{l} \sigma_x = \frac{E}{1-\nu^2} (\varepsilon_x + \nu \varepsilon_y) \\ \sigma_y = \frac{E}{1-\nu^2} (\varepsilon_y + \nu \varepsilon_x) \\ e(\text{dilatation}) = \frac{\Delta V}{V} = \varepsilon_x + \varepsilon_y + \varepsilon_z \end{array} \right\} \left\{ \begin{array}{l} \text{Thin-walled spherical vessel: } \sigma = \frac{pr}{2t} \\ \text{Thin-walled cylindrical vessel: } \left\{ \begin{array}{l} \sigma_{axial} = \frac{pr}{2t} \\ \sigma_{hoop} = \frac{pr}{t} \end{array} \right. \end{array} \right.$$

Deflection & Buckling

$$\left\{ \begin{array}{l} EI \frac{d^2 v}{dx^2} = M \\ \theta(\text{slope}) = \frac{dv}{dx} \end{array} \right\} \left\{ \begin{array}{l} \text{Pinned-Pinned Column } K = 1; \quad \text{Fixed-Free Column } K = 2 \\ \text{Fixed-Fixed Column } K = 0.5; \quad \text{Fixed-Pinned Column } K = 0.699 \end{array} \right\} \Leftrightarrow P_{cr} = \frac{\pi^2 EI}{(KL)^2}$$