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$$FS = \frac{\sigma_y}{\sigma_{allow}} \text{ and } FS = \frac{\tau_y}{\tau_{allow}}; \quad FS = \frac{\sigma_u}{\sigma_{allow}} \text{ and } FS = \frac{\tau_u}{\tau_{allow}}; \quad \sigma = E\varepsilon; \quad \tau = G\gamma$$

$$\sigma = \frac{F}{A}; \quad \tau_{aver} = \frac{F}{A}; \quad \delta = \sum_{i=1}^n \frac{P_i L_i}{E_i A_i}; \quad \delta = \frac{PL}{EA}; \quad \delta = \int_0^L \frac{P(x)}{EA(x)} dx; \quad \nu = \frac{\varepsilon_{lateral}}{\varepsilon_{longitudinal}}$$

$$\left. \begin{array}{l} \text{Power \& Torsion} \\ \left\{ \begin{array}{l} \phi = \frac{TL}{GI_p}; \quad I_p (\text{Solid Shaft of diam. } = d) = \frac{\pi d^4}{32}; \quad I_p (\text{Hollow Shaft } \left\{ \begin{array}{l} d_o : \text{outer diam.} \\ d_i : \text{inner diam.} \end{array} \right\}) = \frac{\pi (d_o^4 - d_i^4)}{32} \\ \tau_{max} = \frac{T(d/2)}{I_p}; \quad \tau = \frac{T\rho}{I_p} \left(\text{where } 0 \leq \rho \leq r = \frac{d}{2} \right); \quad G = \frac{E}{2(1+\nu)}; \quad P(\text{power}) = \omega T; \quad \omega = 2\pi f \end{array} \right. \end{array} \right\}$$

$$\frac{dV}{dx} = -q; \quad \frac{dM}{dx} = V \Leftrightarrow \left\{ \begin{array}{l} \int_A^B dV = V_A - V_B = - \int_A^B q dx = - (\text{Area of the loading diagram bt. A and B}) \\ \int_A^B dM = M_A - M_B = \int_A^B V dx = (\text{Area of the shear-force diagram bt. A and B}) \end{array} \right.$$

$$\kappa (\text{curvature}) = \frac{1}{\rho} = \frac{d\theta}{ds} = \frac{-\varepsilon_x}{y}; \quad \sigma_x = \frac{-M_z y}{I_z}; \quad \tau = \frac{VQ}{Ib}; \quad f = \frac{VQ}{I}; \quad Q = \int y dA$$

$$\left. \begin{array}{l} \text{Mohr's Circle, Stress Trans. \& Princ. Stresses} \\ \left\{ \begin{array}{l} \sigma_{x1}, \sigma_{y1} = \sigma_{aver} \pm \sigma_{diff} \cos(2\theta) \pm \tau_{xy} \sin(2\theta); \quad \sigma_{aver} = \frac{\sigma_x + \sigma_y}{2}; \quad \sigma_{diff} = \frac{\sigma_x - \sigma_y}{2} \\ \tau_{x1y1} = -\sigma_{diff} \sin(2\theta) + \tau_{xy} \cos(2\theta); \quad \sigma_{1,2} = \sigma_{aver} \pm R; \quad R = \sqrt{(\sigma_{diff})^2 + (\tau_{xy})^2} \end{array} \right. \end{array} \right\}$$

Hooke's law for plane stress & vessels:

$$\left\{ \begin{array}{l} \varepsilon_x = \frac{1}{E} (\sigma_x - \nu\sigma_y) \\ \varepsilon_y = \frac{1}{E} (\sigma_y - \nu\sigma_x) \\ \varepsilon_z = \frac{-\nu}{E} (\sigma_y + \sigma_x) \end{array} \right\} \left\{ \begin{array}{l} \sigma_x = \frac{E}{1-\nu^2} (\varepsilon_x + \nu\varepsilon_y) \\ \sigma_y = \frac{E}{1-\nu^2} (\varepsilon_y + \nu\varepsilon_x) \\ e(\text{dilatation}) = \frac{\Delta V}{V} = \varepsilon_x + \varepsilon_y + \varepsilon_z \end{array} \right\} \left\{ \begin{array}{l} \text{Thin-walled spherical vessel: } \sigma = \frac{pr}{2t} \\ \text{Thin-walled cylindrical vessel: } \left\{ \begin{array}{l} \sigma_{axial} = \frac{pr}{2t} \\ \sigma_{hoop} = \frac{pr}{t} \end{array} \right. \end{array} \right.$$

Deflection & Buckling

$$\left\{ \begin{array}{l} EI \frac{d^2 v}{dx^2} = M \\ \theta(\text{slope}) = \frac{dv}{dx} \end{array} \right\} \left\{ \begin{array}{l} \text{Pinned-Pinned Column } K = 1; \quad \text{Fixed-Free Column } K = 2 \\ \text{Fixed-Fixed Column } K = 0.5; \quad \text{Fixed-Pinned Column } K = 0.699 \end{array} \right\} \Leftrightarrow P_{cr} = \frac{\pi^2 EI}{(KL)^2}$$